

# Low-temperature sintering and microwave dielectric properties of LiF-doped $\text{CaMg}_{1-x}\text{Zn}_x\text{Si}_2\text{O}_6$ ceramics

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## Abstract

The diopside ceramics,  $\text{CaMg}_{1-x}\text{Zn}_x\text{Si}_2\text{O}_6$  ( $x=0-0.3$ ), were synthesized via the solid-state reaction method.  $\text{Zn}^{2+}$  substitution for  $\text{Mg}^{2+}$  can markedly lower the densification temperature and improve the microwave dielectric properties of  $\text{CaMgSi}_2\text{O}_6$  ceramics. For  $x=0.1$ ,  $\text{CaMg}_{0.9}\text{Zn}_{0.1}\text{Si}_2\text{O}_6$  ceramics, can be sintered at 1200 °C and exhibit good microwave dielectric properties of  $\epsilon_r=7.88$ ,  $Qf=76,100$  GHz and  $\tau_f=-22.5$  ppm/°C. LiF addition was proved to be effective to lower the sintering temperature to  $\sim 900$  °C without degrading the dielectric properties apparently. The  $\text{CaMg}_{0.9}\text{Zn}_{0.1}\text{Si}_2\text{O}_6$  ceramics doped with 0.6 wt% LiF can be sintered in the temperature range of 900–975 °C and have excellent dielectric properties of  $\epsilon_r\sim 7.7$ ,  $Qf\sim 70,000$  GHz and  $\tau_f\sim -25$  ppm/°C. With low sintering temperature and good dielectric properties, these LiF-doped diopside ceramics are promising materials for LTCC integration applications.

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**Keywords:** C. Microwave dielectric properties; D. Low-temperature co-fired ceramics; D. Silicates

## 1. Introduction

With the rapid development of miniaturized and multi-functional microwave devices, low-temperature co-fired ceramic (LTCC) technology has been playing an increasingly important role in the wireless communication systems and electronic industries. In LTCC devices fabrication, the ceramics are co-fired with highly conductive electrode materials, such as silver (melting point 961 °C) and copper (melting point 1083 °C), to form three-dimensional ceramic modules [1]. Therefore, the ceramics are required to have low sintering temperature which can be co-sinterable with Ag or Cu metal electrodes. Additionally, the low dielectric constant is preferred for dielectric ceramics which can promote the signal propagation speed in ceramic-metal modules. The low dielectric loss (i.e. high quality factor,  $Qf$ ) and small temperature coefficient of resonant frequency ( $\tau_f$ ) are also indispensable properties for LTCCs to ensure low insertion loss and good stability against

temperature change [2–4]. Thus, dielectric microwave components with these attributes mentioned above are identified as one of the best candidates for integrated circuit applications used at a higher frequency.

Recently, a large number of strategies have been reported to lower the densification temperature of ceramics: (a) addition of low melting point materials, such as  $\text{B}_2\text{O}_3$ ,  $\text{Li}_2\text{CO}_3$  and glass [5–7]; (b) chemical processing for smaller particle sizes of starting materials [8]; (c) searching for novel glass-free low-sintering dielectric ceramics [9,10]; and (d) forming solid solutions through ionic substitution [11–13]. The first approach is widely used to lower the densification temperature of commercially available dielectric ceramics because it is the least expensive. However, these low melting point compounds may also have a detrimental effect on the microwave dielectric properties due to the appearance of unexpected secondary phases, which is a major contribution to dielectric loss. It is hence necessary to minimize these phases [14]. As for the last method, the formation of solid solutions can generally modify the dielectric properties of microwave materials, not just lowering the sintering temperature [11,13].

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For example, Pei et al. [11] investigated the substitution of  $\text{Sr}^{2+}$  for  $\text{Ba}^{2+}$  in the  $(\text{Ba}_{1-x}\text{A}_x)\text{La}_4\text{Ti}_4\text{O}_{15}$  ( $\text{A}=\text{Sr}, \text{Ca}$ ) system, which could lower about 100–150 °C and significantly promote the  $Qf$  values with increasing Sr content. Thirumal et al. [13] reported that  $\tau_f$  could be tuned to a near zero value by suitable substitution in the  $\text{Sr}_3\text{Zn}_{1-x}\text{Mg}_x\text{Nb}_2\text{O}_9$  ceramics.

$\text{CaMgSi}_2\text{O}_6$  is a type of inosilicate belonging to the group of clinopyroxenes.  $\text{Ca}^{2+}$  occupies the distorted eight-fold-coordinated  $\text{M}_2$  polyhedra, while  $\text{Mg}^{2+}$  occupies the regular six fold-coordinated  $\text{M}_1$  octahedral sites [15]. More recently,  $\text{CaMgSi}_2\text{O}_6$  ceramics have been demonstrated as a potential candidate material for high-frequency devices fabrication [16–19]. The pure  $\text{CaMgSi}_2\text{O}_6$  ceramic sintered at 1290 °C possessed good microwave dielectric properties, namely  $\epsilon_r$ ,  $Qf$  and  $\tau_f$  were 7.46, 59,638 GHz and  $-46$  ppm/°C, respectively [16]. Several low melting point additions, such as  $\text{B}_2\text{O}_3$ ,  $\text{Li}_2\text{O}-\text{B}_2\text{O}_3-\text{SiO}_2$  and  $\text{Li}_2\text{O}-\text{MgO}-\text{ZnO}-\text{B}_2\text{O}_3-\text{SiO}_2$  glasses, have been considered to lower the sintering temperature of  $\text{CaMgSi}_2\text{O}_6$  [17,18]. However, the relatively high sintering temperature together with low quality factor limited the applications for LTCC-based devices. So, the more effective sintering additives should be searched to obtain the low-fired diopside ceramics with good dielectric properties. Some low melting oxides and fluorides, such as  $\text{ZnO}$  and  $\text{LiF}$ , were reported to be effective as flux in several microwave ceramic systems [20–23].

In the present study, we utilized two steps to obtain the low-temperature co-fired ceramics with excellent dielectric properties in the diopside material system. Firstly,  $\text{Zn}^{2+}$  substituted for  $\text{Mg}^{2+}$  to lower the densification temperature and improve the dielectric properties of  $\text{CaMgSi}_2\text{O}_6$ . Then, a small amount of  $\text{LiF}$  was considered to further lower the sintering temperature to  $\sim 900$  °C. The as-prepared diopside materials exhibited good microwave dielectric properties. In this paper, the effects of  $\text{Zn}^{2+}$  substitution for  $\text{Mg}^{2+}$  and  $\text{LiF}$  addition on the sintering behaviors, microstructure and dielectric properties of  $\text{CaMgSi}_2\text{O}_6$  will be investigated.

## 2. Experimental procedure

The ceramics were prepared using the conventional solid-state method.  $\text{MgO}$  (98.5%),  $\text{CaCO}_3$  (99%),  $\text{ZnO}$  (99.5%),  $\text{SiO}_2$  (99%) and  $\text{LiF}$  (99%) were used as the starting materials. Stoichiometric proportions of the above powders according to the composition of  $\text{CaMg}_{1-x}\text{Zn}_x\text{Si}_2\text{O}_6$  ( $x=0, 0.05, 0.1, 0.15, 0.2$ , and  $0.3$ ) were mixed in ethanol for 4 h with zirconia balls as milling media. The wet mixtures were dried and calcined at 1100 °C for 4 h in air. The calcined powders were re-milled. After drying and sieving, the as-prepared powders together with the organic binder (5 wt% polyvinyl alcohol) were uniaxially pressed under a pressure of 200 MPa into cylinders of 10 mm in diameter and 4–6 mm in thickness. These samples were

sintered in the temperature range of 1100–1300 °C for 4 h in air with the heating rate of 5 °C/min.

Different weight percentages (0.3–3 wt%) of  $\text{LiF}$  powders were considered to further achieve the low-fired  $\text{CaMg}_{1-x}\text{Zn}_x\text{Si}_2\text{O}_6$  ceramics. The  $\text{LiF}$ -containing samples were sintered in the temperature range of 775–1000 °C.

The bulk densities of the sintered ceramics were measured by the Archimedes method. The relative densities were obtained from the bulk and theoretical densities which were calculated from lattice parameters. The crystal phases of the ceramics were characterized by X-ray diffraction (XRD) analysis with a Rigaku D/max-2500 ( $\text{Cu K}\alpha$  radiation, Tokyo, Japan). The microstructures of the sintered ceramics were observed by scanning electron microscopy (SEM, JSM-6301F, JEOL, Tokyo, Japan). A network analyzer (HP8720ES, Hewlett-Packard, Santa Rosa, CA) was used to measure the microwave dielectric properties. The dielectric constants were measured using the Hakki–Coleman [24] post-resonator method by exciting the  $\text{TE}_{011}$  resonant mode of the dielectric resonators using the electric probe of an antenna as suggested by Courtney [25]. The unloaded quality factors were measured using the  $\text{TE}_{018}$  mode in the cavity method [26]. The temperature coefficients of the resonant frequencies of the  $\text{TE}_{011}$  mode were obtained in the temperature range from 25 to 80 °C. The  $\tau_f$  values were calculated by the following relationship:

$$\tau_f = \frac{f_2 - f_1}{f_1(T_2 - T_1)} \quad (1)$$

where  $f_1$  and  $f_2$  are the resonant frequency at  $T_1$  and  $T_2$ , respectively.

## 3. Results and discussion

### 3.1. $\text{CaMg}_{1-x}\text{Zn}_x\text{Si}_2\text{O}_6$ ceramics

X-ray diffraction experiments were performed on the well-sintered  $\text{CaMg}_{1-x}\text{Zn}_x\text{Si}_2\text{O}_6$  ceramics, and the results are shown in Fig. 1. It can be noted that the XRD patterns for all samples can be identified as diopside structure similar to the  $\text{CaMgSi}_2\text{O}_6$  compound (JCPDS 19-0239).  $\text{CaMgSi}_2\text{O}_6$  and  $\text{CaZnSi}_2\text{O}_6$  are chain silicates, crystallizing in monoclinic symmetry with a space group of  $\text{C2/c}$ . It was reported that they can form quaternary solid solutions together with  $\text{CaFeSi}_2\text{O}_6$  and  $\text{CaMnSi}_2\text{O}_6$  [15]. Moreover, the ionic radius of  $\text{Zn}^{2+}$  (0.736 Å, CN=6) is nearly close to  $\text{Mg}^{2+}$  (0.728 Å, CN=6) [27], making it easy to substitute the magnesium site by the zinc ion. Thus, the solid solutions of  $\text{CaMg}_{1-x}\text{Zn}_x\text{Si}_2\text{O}_6$  seemed to be easily formed. And yet, some peaks of  $\text{Ca}_2\text{ZnSi}_2\text{O}_7$  hardystonite phase (JCPDS 35-0745) appear in the samples of  $x=0.2$  and  $0.3$ , implying the limited solid solutions formed from  $\text{CaMgSi}_2\text{O}_6$  and  $\text{CaZnSi}_2\text{O}_6$  end compounds. These results suggest that the solid solutions of  $\text{CaMg}_{1-x}\text{Zn}_x\text{Si}_2\text{O}_6$  can be formed in the sintered bodies with a small amount of  $\text{Zn}^{2+}$  substitution for  $\text{Mg}^{2+}$ .

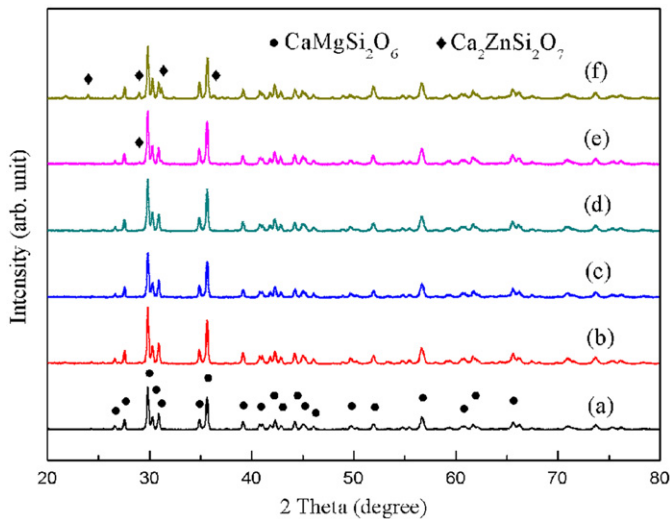


Fig. 1. XRD patterns of well-sintered  $\text{CaMg}_{1-x}\text{Zn}_x\text{Si}_2\text{O}_6$  ( $x=0, 0.05, 0.1, 0.15, 0.2$ , and  $0.3$ ) ceramics.

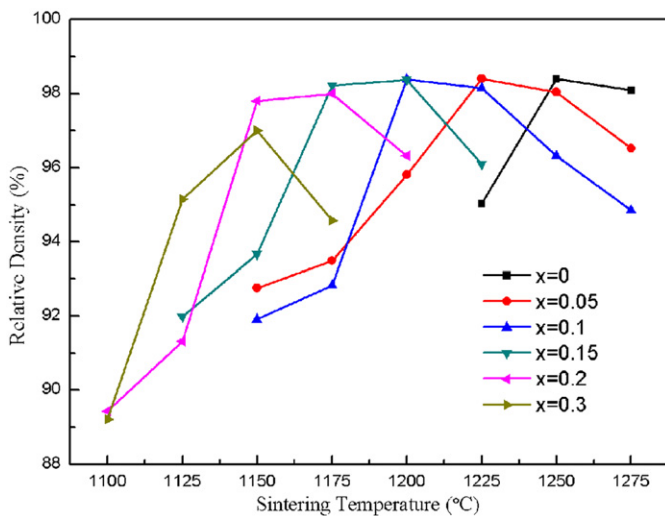


Fig. 2. Relative densities of  $\text{CaMg}_{1-x}\text{Zn}_x\text{Si}_2\text{O}_6$  ceramics as a function of sintering temperature.

The relative densities of  $\text{CaMg}_{1-x}\text{Zn}_x\text{Si}_2\text{O}_6$  ceramics as a function of sintering temperature are shown in Fig. 2. For each composition, the relative densities initially increase with increasing temperature and then decrease after reaching a maximum value, through which the optimized sintering temperatures of the ceramics were determined, i.e.  $1250^\circ\text{C}$  for  $x=0$ ,  $1225^\circ\text{C}$  for  $x=0.05$ ,  $1200^\circ\text{C}$  for  $x=0.1$ ,  $1175^\circ\text{C}$  for  $x=0.15$ , and  $1150^\circ\text{C}$  for  $x=0.2$  and  $x=0.3$ . It is clear that a higher  $\text{Zn}^{2+}$  content shifts the obtainable maximum density to a lower temperature. This result implies that the substitution of  $\text{Zn}^{2+}$  for  $\text{Mg}^{2+}$  can markedly lower the sintering temperature in the  $\text{CaMg}_{1-x}\text{Zn}_x\text{Si}_2\text{O}_6$  system.

The microstructure observations were performed on the well-sintered  $\text{CaMg}_{1-x}\text{Zn}_x\text{Si}_2\text{O}_6$  ceramic samples by scanning electron microscopy, and the typical micrographs are shown in Fig. 3. All samples have dense microstructures

with low porosity. As shown in Fig. 3(a), the average grain size of pure  $\text{CaMgSi}_2\text{O}_6$  is about  $1\mu\text{m}$  except some abnormal growth grains. It can be also seen that pores exist in these abnormally grown grains. These phenomena may be due to the fast growth of the grains, thereby some pores were been trapped in the bodies of the abnormal growth grains [4]. As shown in Fig. 3(b), the grain sizes are more uniform and hardly any pore is observed in the large grains. It is interesting to note that the sample with  $x=0.1$  seems to possess a homogeneous microstructure with equiaxed grains in Fig. 3(c). This might be related to the improvement of the sintering process caused by the formation of solid solutions [20]. However, the abnormal grain growth reappears for the sample  $x=0.15$  in Fig. 3(d), probably because of the fast growth of the grains by excessive amount of  $\text{Zn}^{2+}$  substitution for  $\text{Mg}^{2+}$ .

The microwave dielectric properties of  $\text{CaMg}_{1-x}\text{Zn}_x\text{Si}_2\text{O}_6$  ceramics were characterized as a function of sintering temperature and  $\text{Zn}^{2+}$  content, and the results are shown in Fig. 4 and Table 1. For each composition (see Fig. 4(a, b)), the relationship between dielectric properties ( $\epsilon_r$  and  $Qf$  values) and sintering temperature share the similar trend with that between density and sintering temperature. According to Penn et al. [28], porosity plays a significant role in the dielectric properties ( $\epsilon_r$  and  $Qf$  values) of microwave materials. Generally, both  $\epsilon_r$  and  $Qf$  values decrease with increasing porosity volume, while pores directly lower the densities. In this case,  $\epsilon_r$  and  $Qf$  increase with densification [11].

To better know the effects of secondary phase on the microwave dielectric properties of  $\text{CaMgSi}_2\text{O}_6$ -based ceramics,  $\text{Ca}_2\text{ZnSi}_2\text{O}_7$  ceramics were also synthesized in the present work. When sintered at  $1325^\circ\text{C}$ , the ceramic shows an  $\epsilon_r$  of 10.2,  $Qf$  of 14,000 GHz and  $\tau_f$  of  $-30.0\text{ ppm}/^\circ\text{C}$ .

It can be seen from Fig. 4(a), that the maximum  $\epsilon_r$  values increase from 7.80 to 7.99 as  $x$  varies from 0 to 0.15. In the case of microwave dielectrics, the dielectric constant is intrinsically determined by ionic polarizability [3,28]. Shannon [29] reported that the polarizability of  $\text{Zn}^{2+}$  ( $2.09\text{ \AA}^3$ ) is larger than that of  $\text{Mg}^{2+}$  ( $1.33\text{ \AA}^3$ ), thereby  $\epsilon_r$  increases in the solid solution series [30]. Beyond the solid solution limit,  $\text{Ca}_2\text{ZnSi}_2\text{O}_7$  has a larger dielectric constant than  $\text{CaMgSi}_2\text{O}_6$ , the appearance of which causes  $\epsilon_r$  to increase in the samples of  $x=0.2$  and  $0.3$ . These results basically agreed with the well-known Lichtenecker empirical rule [31].

The dielectric loss is found to depend very strongly on pore volume, purity, and grain size [28]. To better interpret the variation of  $Qf$  values with  $\text{Zn}^{2+}$  content, the  $Qf$  values of representative samples are listed in Table 1. As the relative densities of these samples are all above 96%, the effect of porosity on the dielectric loss can be neglected [5]. In this case, the grain size and unexpected impurities mainly dominate the dielectric loss. Among  $\text{CaMg}_{1-x}\text{Zn}_x\text{Si}_2\text{O}_6$  solid solutions ( $x=0-0.15$ ), no secondary phase was observed from Fig. 1. So the effect of impurities on the dielectric loss can be also neglected. It is worthy to note



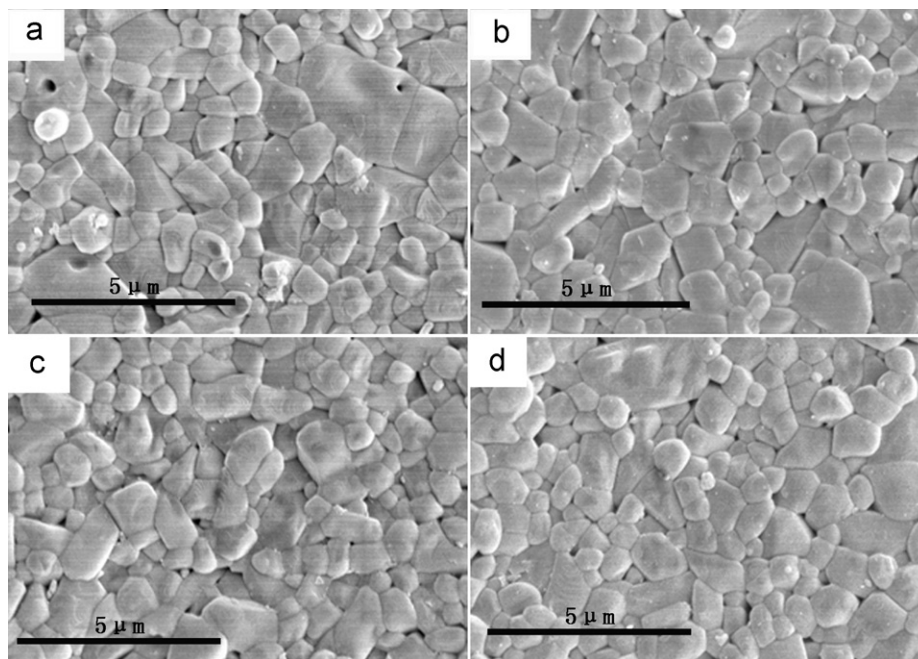


Fig. 3. SEM micrographs of the surfaces of well-sintered  $\text{CaMg}_{1-x}\text{Zn}_x\text{Si}_2\text{O}_6$  ceramics: (a)  $x=0$ , 1250 °C, (b)  $x=0.05$ , 1225 °C, (c)  $x=0.1$ , 1200 °C, and (d)  $x=0.15$ , 1175 °C.

that  $\text{CaMg}_{0.9}\text{Zn}_{0.1}\text{Si}_2\text{O}_6$  ceramic has the highest  $Qf$  value due to its homogeneous microstructure with equiaxed grains, which leads to decrease in the inevitable pores caused by the abnormally grown grains and thereby lowering the dielectric loss. This results are consistent with the pertinent literatures [20,32]. Beyond the solid solution limit,  $Qf$  values degrade rapidly from 61,400 GHz to 37,200 GHz as  $x$  varies from 0.2 to 0.3, owing to the fact that the  $\text{Ca}_2\text{ZnSi}_2\text{O}_7$  phase has a very low  $Qf$  value of 14,000 GHz and deteriorates the quality factors of diopside ceramics consequently.

Meanwhile, the variations of  $\tau_f$  with  $\text{Zn}^{2+}$  content are also given in Fig. 4(c) and Table 1. The  $\tau_f$  initially shows no remarkable variations when  $x$  increases from 0 to 0.15, and then slightly decreases to more negative values. The result is closely related to  $\text{Ca}_2\text{ZnSi}_2\text{O}_7$  (−30.0 ppm/°C) has a little more negative  $\tau_f$  than that of  $\text{CaMgSi}_2\text{O}_6$  (−24.1 ppm/°C).

### 3.2. $\text{CaMg}_{0.9}\text{Zn}_{0.1}\text{Si}_2\text{O}_6 + y \text{ wt\% LiF}$ ceramics

A small amount of LiF was considered as a sintering assistant to further lower the sintering temperature of  $\text{CaMg}_{0.9}\text{Zn}_{0.1}\text{Si}_2\text{O}_6$  ceramics. The bulk densities of LiF-doped  $\text{CaMg}_{0.9}\text{Zn}_{0.1}\text{Si}_2\text{O}_6$  ceramics sintered under various conditions are shown in Fig. 5. The concentration of LiF strongly influences the density. Doped with 0.6 wt% LiF, the optimal sintering temperature is significantly lowered from 1200 °C to 975 °C. With increasing LiF content from 0.6 wt% to 3 wt%, the sintering temperature at which the maximum densities occur decreases from 975 °C to 800 °C. This result suggests that LiF is a very effective sintering additive for  $\text{CaMg}_{0.9}\text{Zn}_{0.1}\text{Si}_2\text{O}_6$  ceramics. It can be

ascribed to the fact that LiF (melting point 845 °C) can melt to form a liquid phase to promote the densification process of  $\text{CaMg}_{0.9}\text{Zn}_{0.1}\text{Si}_2\text{O}_6$ , thereby significantly lowering the sintering temperature and enhancing the sintering behaviors [23]. In general, Fig. 5 shows a decrease in density at higher LiF contents, probably due to liquid phase sintering in the presence of molten LiF and the volatilization of LiF. It is reported that the porous microstructure can be also caused by volatilization of the lithium salt [33], thereby decreasing the apparent density and degrading the dielectric properties consequently. It can be also noted that LiF addition broadens the process window, which will be highly beneficial for practical LTCC applications.

Fig. 6 shows the XRD patterns of  $\text{CaMg}_{0.9}\text{Zn}_{0.1}\text{Si}_2\text{O}_6$  ceramics doped with different amounts of LiF. Hardly any additional phase is present other than the  $\text{CaMgSi}_2\text{O}_6$  phase in 0.6 wt% LiF-doped ceramics sintered at 900 °C and higher to 1000 °C. From Fig. 6(c), new peaks of  $\text{Li}_{0.6}\text{Zn}_{1.1}\text{Si}_{1.3}\text{O}_4$  (JCPDS 34-1231) are observed in 3 wt% LiF-doped sample sintered at 900 °C, which indicates that the reactions between LiF and matrix material take place during the sintering process, leading to degradation of the apparent density and the dielectric properties [33].

Fig. 7 shows the SEM micrographs of 0.6 wt% LiF-doped  $\text{CaMg}_{0.9}\text{Zn}_{0.1}\text{Si}_2\text{O}_6$  ceramics sintered at different temperatures. From Fig. 7(a), some pores can be observed on the sample surface. These pores could be related to the poor densification with low temperature. Dense microstructures with low porosity can be observed in Fig. 7(b,c), which is related to the grain growth with increasing sintering temperature. Compared with pure  $\text{CaMg}_{0.9}\text{Zn}_{0.1}\text{Si}_2\text{O}_6$  ceramics shown in Fig. 3(c), the average grain size slightly

increases by doping 0.6 wt% LiF. This could be due to the effect of low melting point of LiF on the grain growth behavior of  $\text{CaMg}_{0.9}\text{Zn}_{0.1}\text{Si}_2\text{O}_6$  ceramics.

The microwave dielectric properties of LiF-doped  $\text{CaMg}_{0.9}\text{Zn}_{0.1}\text{Si}_2\text{O}_6$  ceramics are shown in Fig. 8 and Table 2. As for glass added ceramics, the microwave dielectric properties are more likely relying on density and the presence of secondary phases [7,18]. Likewise, the variations of  $\epsilon_r$  and  $Qf$  values with sintering temperature nearly follow the similar trend with the relationship

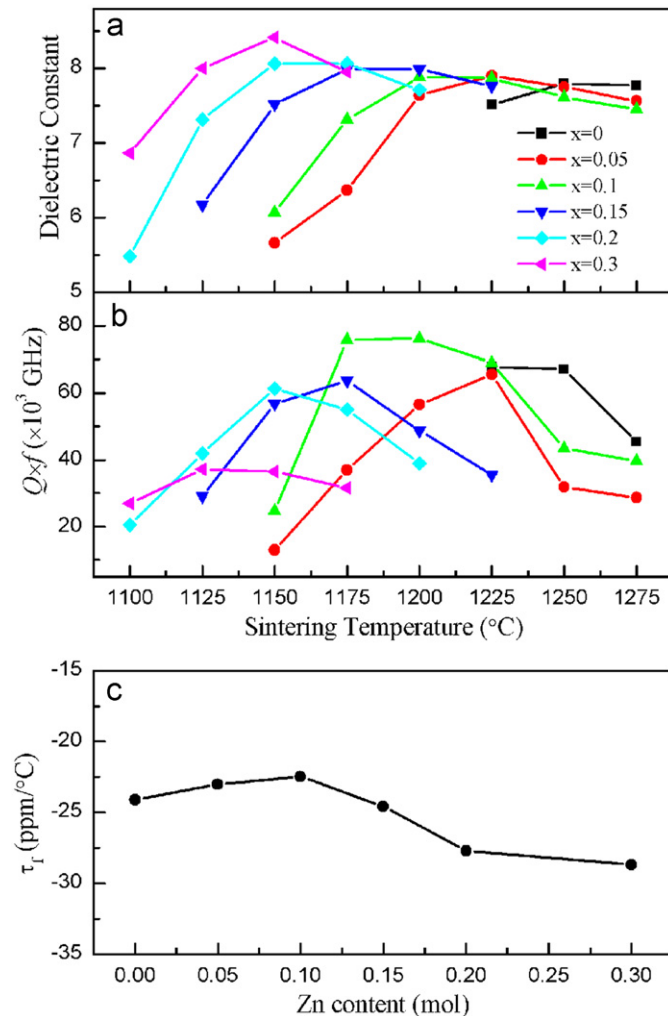


Fig. 4. Microwave dielectric properties of  $\text{CaMg}_{1-x}\text{Zn}_x\text{Si}_2\text{O}_6$  ceramics: (a)  $\epsilon_r$ , (b)  $Qf$  vs. sintering temperature, and (c)  $\tau_f$  vs. Zn content.

Table 1

Relative densities and microwave dielectric properties of  $\text{CaMg}_{1-x}\text{Zn}_x\text{Si}_2\text{O}_6$  ceramics sintered at optimized temperatures.

Samples, $x$	Sintering temperature (°C)	Relative density (%)	$\epsilon_r$	$Qf$ (GHz)	$\tau_f$ (ppm/°C)
0	1250	98.39	7.80	67,100	−24.1
0.05	1225	98.40	7.90	65,600	−23.0
0.10	1200	98.38	7.88	76,100	−22.5
0.15	1175	98.22	7.99	63,700	−24.6
0.20	1150	97.80	8.06	61,400	−27.7
0.30	1150	97.00	8.41	36,400	−28.7

between bulk densities and sintering temperature. As shown in Fig. 8(a, b) and Table 2,  $\epsilon_r$  and  $Qf$  values decrease with increasing amount of LiF addition. This result might be due to the volatility of lithium and the unexpected secondary phases [33]. Especially for the

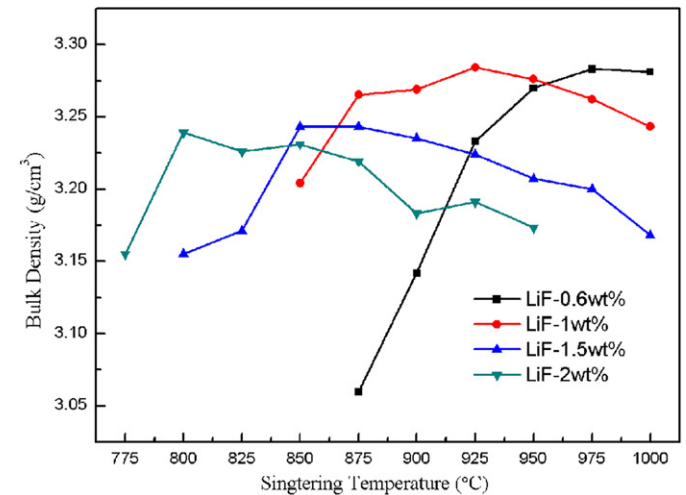


Fig. 5. Bulk densities of LiF-doped  $\text{CaMg}_{0.9}\text{Zn}_{0.1}\text{Si}_2\text{O}_6$  ceramics as a function of sintering temperature.

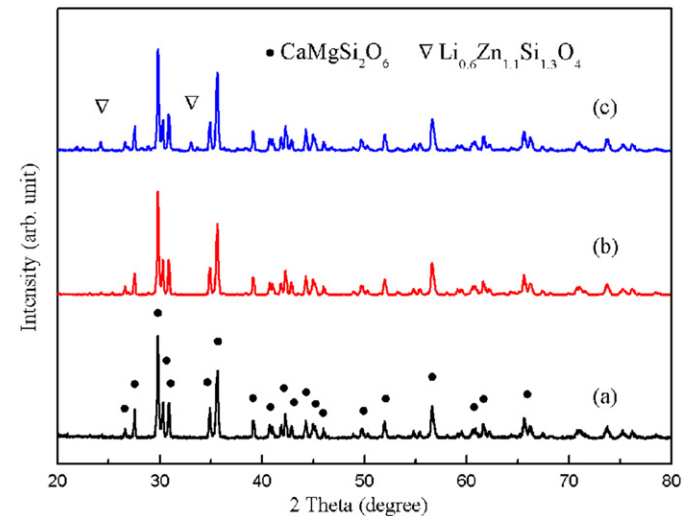


Fig. 6. XRD patterns of LiF-doped  $\text{CaMg}_{0.9}\text{Zn}_{0.1}\text{Si}_2\text{O}_6$  ceramics: (a) 0.6 wt% LiF, 900 °C, (b) 0.6 wt% LiF, 1000 °C, and (c) 3 wt% LiF, 900 °C.

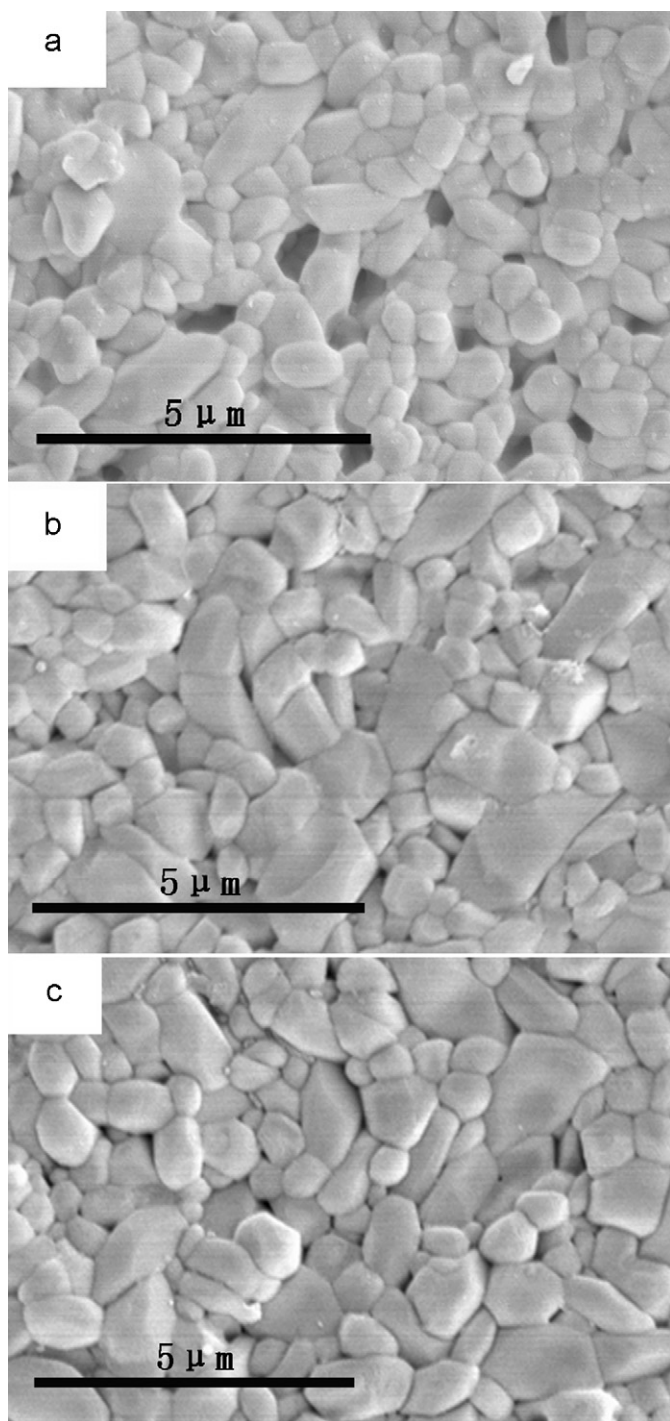


Fig. 7. SEM micrographs of the surfaces of 0.6 wt% LiF-doped  $\text{CaMg}_{0.9}\text{Zn}_{0.1}\text{Si}_2\text{O}_6$  ceramics sintered at different temperatures: (a) 900 °C, (b) 925 °C, and (c) 950 °C.

samples added with excess amount of 2 wt% LiF, the quality factor almost becomes independent of sintering temperature, which seriously degrades to about 24,000 GHz because of the appearance of  $\text{Li}_{0.6}\text{Zn}_{1.1}\text{Si}_{1.3}\text{O}_4$ . From Fig. 8(c),  $\tau_f$  basically decreases nonlinearly to more negative values as  $x$  increases. These results can be closely related to the  $\text{Li}_{0.6}\text{Zn}_{1.1}\text{Si}_{1.3}\text{O}_4$  phase which might have a more negative  $\tau_f$ .

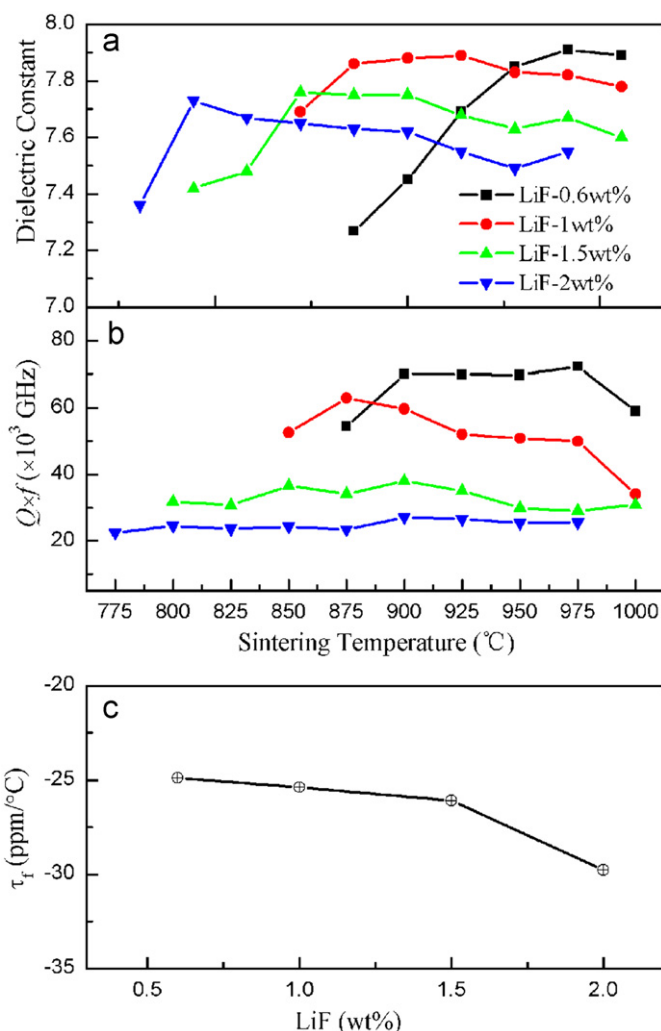


Fig. 8. Microwave dielectric properties of LiF-doped  $\text{CaMg}_{0.9}\text{Zn}_{0.1}\text{Si}_2\text{O}_6$  ceramics: (a)  $\epsilon_r$ , (b)  $Qf$  vs. sintering temperature, and (c)  $\tau_f$  vs. LiF content.

It is noteworthy that 0.6 wt% LiF-doped  $\text{CaMg}_{0.9}\text{Zn}_{0.1}\text{Si}_2\text{O}_6$  ceramics, sintered in the temperature range of 900–975 °C, maintain relatively high  $Qf$  values about 70,000 GHz. As no apparent peaks of secondary phases were examined from XRD patterns in Fig. 6(a, b), these samples hence possess relatively high  $Qf$  values. These results indicate that a small amount of LiF can effectively decrease the sintering temperature without degrading the microwave dielectric properties of host materials. It is obvious that these ceramics are promising to be co-fired with Ag electrode materials for further LTCC applications.

#### 4. Conclusions

In this work, we utilized two steps to obtain the low-temperature co-fired ceramics with excellent dielectric properties in the diopside material system. Firstly,  $\text{CaMg}_{1-x}\text{Zn}_x\text{Si}_2\text{O}_6$  solid solutions through  $\text{Zn}^{2+}$  substitution for  $\text{Mg}^{2+}$  can markedly lower the sintering temperature and enhance the microwave dielectric properties.

Table 2

Bulk densities and microwave dielectric properties of  $\text{CaMg}_{0.9}\text{Zn}_{0.1}\text{Si}_2\text{O}_6 + y \text{ wt\% LiF}$  ceramics.

$y$ (wt%)	Sintering temperature ( $^{\circ}\text{C}$ )	Bulk density ( $\text{g}/\text{cm}^3$ )	$\epsilon_r$	$Qf$ (GHz)	$\tau_f$ (ppm/ $^{\circ}\text{C}$ )
0.6	925	3.270	7.69	69,900	−24.9
1	900	3.269	7.88	59,700	−25.4
1.5	850	3.243	7.76	36,500	−26.1
2	850	3.231	7.65	24,300	−29.8

$\text{CaMg}_{0.9}\text{Zn}_{0.1}\text{Si}_2\text{O}_6$  ceramic exhibits good dielectric properties of  $\epsilon_r = 7.88$ ,  $Qf = 76,100$  GHz and  $\tau_f = -22.5$  ppm/ $^{\circ}\text{C}$ . Then, LiF was considered to further reduce the densification temperature of  $\text{CaMg}_{0.9}\text{Zn}_{0.1}\text{Si}_2\text{O}_6$  ceramics. A small amount of LiF addition can lower the sintering temperature prominently. In particular, 0.6 wt% LiF-doped  $\text{CaMg}_{0.9}\text{Zn}_{0.1}\text{Si}_2\text{O}_6$  ceramics can be sintered in the temperature range of 900–975  $^{\circ}\text{C}$  and have relatively high  $Qf$  values of  $\sim 70,000$  GHz. These materials possess a pretty wide process window, promising to be the potential candidates for LTCC applications.

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