

# Microstructural design of BaTiO<sub>3</sub>-based ceramics for temperature-stable multilayer ceramic capacitors

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## Abstract

In order to satisfy EIA X8R specification, a new type of BaTiO<sub>3</sub>-based ceramic with hierarchical structure in a formula scheme “a ferroelectric ABO<sub>3</sub> + another ferroelectric ABO<sub>3</sub>”, was designed. There were (Ba, Bi)TiO<sub>3</sub> and Ba(Ti, Zr)O<sub>3</sub> phases with different Curie temperatures coexisting in the grains from inside to outside, prepared by wet chemical method under 100 °C. The hierarchical structure of the ceramic grains was proved by X-ray diffraction (XRD), scanning electron microscopy (SEM) and energy dispersive X-ray spectroscopy (EDX). The dielectric constant of (Ba, Bi)TiO<sub>3</sub>–Ba(Ti, Zr)O<sub>3</sub> ceramic was ~6000, the  $\Delta C/C_{20\text{ }^{\circ}\text{C}}$  was –12.0%, 14.1%, and –8.3% at –55 °C, 130 °C, and 160 °C, respectively, and the dielectric loss is less than 0.1, which is obviously superior to (Ba, Bi)TiO<sub>3</sub> and Ba(Ti, Zr)O<sub>3</sub>. The results of this work showed that the formula scheme “a ferroelectric ABO<sub>3</sub> + another ferroelectric ABO<sub>3</sub>” for solid solutions is a promising approach to prepare high performance temperature-stable capacitor materials.

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## 1. Introduction

Multilayer ceramic capacitors (MLCCs) are one of the most important electronic components because of their economical volumetric efficiency for capacitance and high reliability. High performance MLCCs require high dielectric constant and good stability as the market drives electronic devices toward ever-greater miniaturization and multifunctionality [1]. Due to the potential applications in a wide range of electronic devices, such as multilayer ceramic capacitors, transducers, infrared detectors, and pulse generating devices [2,3], the crystal structure, ferroelectric phase transition, dielectric properties of BaTiO<sub>3</sub> and related BaTiO<sub>3</sub>-based ceramics have been extensively investigated. Many studies have been carried out to investigate the dielectric temperature-stability of BaTiO<sub>3</sub>

ceramic in a comparatively wide temperature range [4–6], because electronic parts in the control module for automotive uses must keep their performance under high temperature [7]. Many BaTiO<sub>3</sub>-based X7R multilayer ceramic capacitors (MLCCs) have been widely used for miniaturization of electronic components attributed to their temperature-stable dielectric behavior, namely the variation of capacity ( $\Delta C/C_{20\text{ }^{\circ}\text{C}}$ ) less than  $\pm 15\%$  over the temperature range from –55 to 125 °C (upper working temperature 125 °C). However, there is increasing need to extend the working range of these devices to 150 °C to achieve X8R specification [8].

Pure BaTiO<sub>3</sub> is a ferroelectric perovskite (ABO<sub>3</sub>) with a high room temperature permittivity (~2000–3000) and a modest Curie temperature,  $T_C \sim 130\text{ }^{\circ}\text{C}$  [4]. When temperature is higher than 130 °C, the permittivity will drop dramatically so that the material cannot be used sequentially at this temperature. At this time, the temperature dependence of capacitance change illustrates the so-called “clockwise effect” [9]. The growing trend is to reduce dielectric thickness and increased stacking of electrode layers to meet miniaturization of electronic components [10]. However, the clockwise effect

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will be remarkable with the reduced thickness, namely the dielectric properties of MLCC will be exacerbated at the temperature higher than 130 °C [11]. Thus extending the range of BaTiO<sub>3</sub> ceramic usage scope to high temperature is essential to realize X8R MLCC materials.

In order to improve the temperature coefficient of BaTiO<sub>3</sub>, various works have been focused on the preparation of the BaTiO<sub>3</sub>-based ceramic powder with core-shell structure by the traditional solid-phase method, through adulteration of chemical nonuniformity, e.g. mixing BaTiO<sub>3</sub> powder with some oxides, such as rare earth oxides, Nb<sub>2</sub>O<sub>5</sub>, Co<sub>2</sub>O<sub>3</sub>, and Bi<sub>2</sub>O<sub>3</sub> [12,13]. Namely, the ceramic crystal is comprised of two parts: pure BaTiO<sub>3</sub> as grain core (ferroelectric tetragonal phase) and oxide-doped BaTiO<sub>3</sub> as grain shell (paraelectric cubic phase), with the transition region between the core and the shell [14]. However, the dielectric constant of barium titanate-based ceramic materials is greatly dependent on the ferroelectric tetragonal phase. It is well-known that the permittivity of BaTiO<sub>3</sub> capacitor will decrease remarkably when it is turned from the ferroelectric tetragonal phase into paraelectric cubic phase. Recently, bismuth-based dielectric ceramics have been broadly studied for its relatively low sintering temperature (less than 1000 °C), high dielectric constant and have been investigated for the application as multilayer capacitors [15,16]. Zr<sup>4+</sup> modified BaTiO<sub>3</sub> ceramic exhibits a high dielectric constant, a low dissipation and ability to shift  $T_C$  to a low temperature [17–19].

In this paper, we reported a new structure type of BaTiO<sub>3</sub> ceramic crystal with hierarchical structure. The crystal grain consists of several BaTiO<sub>3</sub>-based phases with different chemical compositions in a formula scheme “a ferroelectric ABO<sub>3</sub> + another ferroelectric ABO<sub>3</sub>”, from inside to outside. Each phase has specific Curie temperature and Curie peak, according to different dopants prepared by wet chemical method. There are two Curie peaks at high-temperature region and low-temperature region, respectively in the whole scope of working temperature. The temperature stability will be greatly improved after multiplying of those Curie peaks, presenting multi-peak effect. Meanwhile, the permittivity of the material can maintain a high level by choosing proper doping elements. This enables extensive tailoring of their dielectric properties by choosing an appropriate BaTiO<sub>3</sub>-based phase with specific  $T_C$  and dielectric constant. In the present investigation, (Ba<sub>0.985</sub>Bi<sub>0.01</sub>)TiO<sub>3</sub>–Ba(Ti<sub>0.9</sub>Zr<sub>0.1</sub>)O<sub>3</sub> (abbreviated BBT–BTZ) powder and ceramic were synthesized, and the microstructures and dielectric properties of (Ba<sub>0.985</sub>Bi<sub>0.01</sub>)TiO<sub>3</sub>–Ba(Ti<sub>0.9</sub>Zr<sub>0.1</sub>)O<sub>3</sub> ceramics were thus measured. (Ba<sub>0.985</sub>Bi<sub>0.01</sub>)TiO<sub>3</sub> (BBT) and Ba(Ti<sub>0.9</sub>Zr<sub>0.1</sub>)O<sub>3</sub> (BTZ) ceramic were also prepared for contrast examinations.

## 2. Experimental procedure

### 2.1. Preparation of BBT powder

The BBT powder studied was prepared using liquid-state method with Bi<sub>2</sub>O<sub>3</sub>, TiCl<sub>4</sub> and Ba(OH)<sub>2</sub>·8H<sub>2</sub>O (AR 99.0% China) as raw materials. Firstly, TiCl<sub>4</sub> was hydrolyzed in

stoichiometric Bi<sub>2</sub>O<sub>3</sub> hydrochloric acid solution to form a transparent solution. Then Ba(OH)<sub>2</sub>·8H<sub>2</sub>O was dissolved in boiling water and mixed with the above solution in a flask to form a homogeneous solution. Secondly, the mixture was heated to 95–100 °C by a heating jacket with vigorous and continuous stirring for 4 h. The reaction product then was obtained after washing and drying in the air.

### 2.2. Preparation of BBT–BTZ powder

ZrOCl<sub>4</sub>·8H<sub>2</sub>O, TiCl<sub>4</sub>, Ba(OH)<sub>2</sub>·8H<sub>2</sub>O (AR 99.0% China) and the aforementioned BBT were used as starting materials. Firstly, TiCl<sub>4</sub> was hydrolyzed in stoichiometric ZrOCl<sub>4</sub> hydrochloric acid solution, and mixed with Ba(OH)<sub>2</sub> boiling water solution in a flask to form a homogeneous solution by stirring. Secondly, BBT was put into the three-necked flask and mixed with the solution together, reacted in 95–100 °C for 4 h. Then BTZ would grow at the surface of BBT, because the similarity of their geometrical structure enabled BBT as seed crystal to induce the growth of BTZ on the surface. It will be proved by the following characterizations.

### 2.3. Preparation of BBT–BTZ ceramics

The prepared ceramic powders were pressed in disk form (20 mm in diameter and 2 mm in thickness) using 8 wt% of PVA as a binder. After discharging binder, the disks were finally fired at 1100 °C for 1 h in air. Silver paste was fired on both sides of the samples at 550 °C for 10 min as electrodes.

Dielectric measurements of the samples were performed by using a LCR meter at 1 kHz in the temperature range from –55 °C to 180 °C. Phase analysis is carried out by X-ray diffraction (XRD) technique using the Cu K $\alpha$  radiation of D8 Advance. Scanning electron micrographs (SEM) is recorded with a Jeol 940A electron microscope. A point-to-point nano-analysis has been done using scanning transmission electron microscope (STEM) with energy dispersive X-ray spectroscopy (EDX) facility.

## 3. Results and discussion

Fig. 1 shows the XRD patterns for all the doped BaTiO<sub>3</sub> compositions of BTZ, BBT, and BBT–BTZ. These XRD patterns were measured on the sintered ceramic pellets. There was no trace of secondary peak in BTZ and BBT patterns (Fig. 1a and b), which suggests the formation of homogeneous solid solution with perovskite phase. It is evident that XRD peaks of BBT shift to a large angle, which indicates the decrease of lattice parameters. It is due to the radius of Bi<sup>3+</sup> (0.103 nm) smaller than that of Ba<sup>2+</sup> (0.135 nm), which occupies Ba-site. Instead, the XRD peaks of BTZ shift toward small angle, which is attributed that the radius of Zr<sup>4+</sup> (0.072 nm) is larger than that of Ti<sup>4+</sup> (0.060 nm). The ionic radii used are those of Shannon [20,21]. However, BBT–BTZ shows two peaks in each peak position, which belongs to BBT and BTZ, respectively according to the relative shift to the peak position of pure BaTiO<sub>3</sub>. It is observed obviously in Fig. 2. This

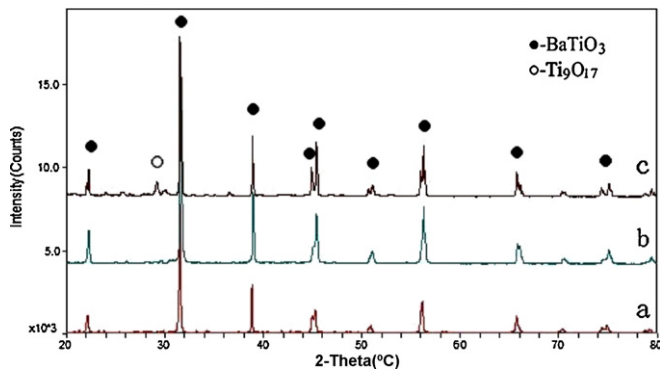


Fig. 1. XRD patterns of BaTiO<sub>3</sub>-based ceramic: (a) BTZ, (b) BBT, and (c) BBT–BTZ.

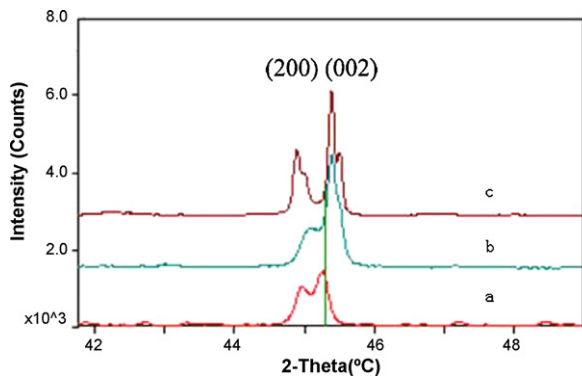


Fig. 2. XRD peaks at  $2\theta = 45.294^\circ$  of (a) BTZ, (b) BBT, and (c) BBT–BTZ (the vertical line represents the peak position of pure BaTiO<sub>3</sub>).

result indicates there are two different phases of BBT and BTZ coexisting in BBT–BTZ ceramic. The secondary phase is observed by XRD in BBT–BTZ, which is proved to be Ti<sub>9</sub>O<sub>17</sub>. The reasons for the emergence of Ti<sub>9</sub>O<sub>17</sub> will be discussed in another paper. The  $c/a$  ratio and volume of the unit cell were calculated, shown in Table 1.

The (0 0 2) and (2 0 0) diffraction peaks of the BaTiO<sub>3</sub> solid solution for the determination of the crystal system are shown in Fig. 2. The (0 0 2) and (2 0 0) diffraction lines are separated from each other with the addition of Bi, Zr, which suggests BBT and BTZ exhibited tetragonal structure.

Table 1

The  $c/a$  ratio and unit cell volume of BBT, BTZ and BBT–BTZ.

Sample	BBT	BTZ	BBT–BTZ
$c/a$ ratio	1.000577	1.000684	1.008771
Unit cell volume (nm <sup>3</sup> )	64.07478	64.5753	64.31962

Table 2

Dielectric properties of BBT, BTZ and BBT–BTZ.

Temperature (°C)	Dielectric constant			Dielectric loss of BBT–BTZ
	BBT	BTZ	BBT–BTZ	
–55	946	1435	4501	0.01
–40	985	1500	4700	0.01
–20	1000	1745	4803	0.016
0	1022	1821	4871	0.032
20	1025	2139	5117	0.055
40	1038	2778	5439	0.082
60	1123	2971	5669	0.093
80	1263	2818	5744	0.039
100	1530	2443	5546	0.031
120	2254	2028	5723	0.02
140	2758	1749	5482	0.03
160	2102	1521	4688	0.013

The relative density of BBT and BBT–BTZ pellets sintered at 1100 °C are ~95–98%, which shows good sintering properties. Fig. 3a is the SEM photo of BBT, with an average grain size of 300 nm. Fig. 3b is the SEM photo of BBT–BTZ, with an average grain size of ~1 μm. There is no secondary phase detected in both photos. Considering the XRD pattern of BBT–BTZ in which BBT and BTZ coexist (the content of Ti<sub>9</sub>O<sub>17</sub> is too little to be calculated), it is believed that BTZ is grown on the BBT surface to form hierarchical structure.

Fig. 4 illustrates STEM/EDX point-to-point analyses across the diameter of grain for BBT–BTZ. The result suggests that the content of Bi<sup>3+</sup> is higher and the content of Zr<sup>4+</sup> is lower at the grain core than that of those at grain shell, which indicates that BBT is coated by BTZ. The results are in good agreement with XRD and SEM.

The dielectric constant and dissipation data of BBT, BTZ and BBT–BTZ samples are shown in Table 2. The maximum

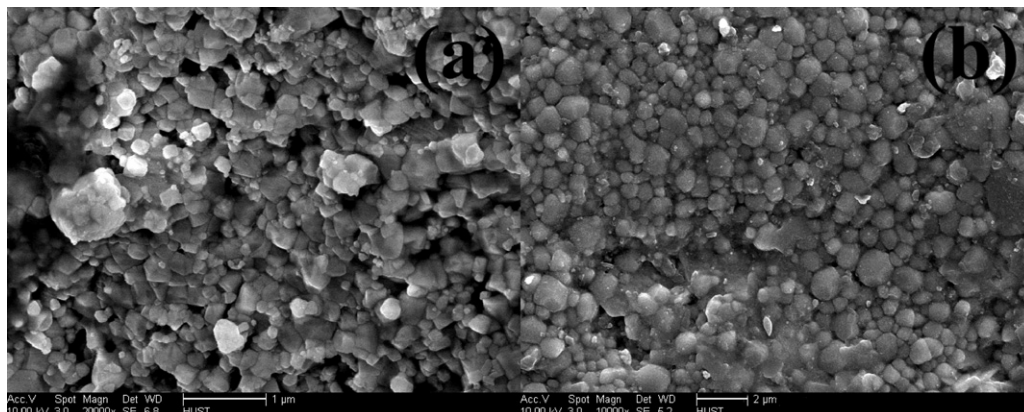


Fig. 3. SEM photos of (a) BBT and (b) BBT–BTZ.

dielectric constant is up to  $\sim 6000$  and dissipation is less than 0.1. Fig. 5 depicts the temperature dependences of capacitance change ( $\varepsilon$ - $T$  curve) of BBT, BTZ, BBT–BTZ samples, while the fitting curve of BBT and BTZ (nominated as fitting-BBT–BTZ) is drawn for comparison. As the figure shows, addition of Zr element to  $\text{BaTiO}_3$  gives a movement of  $T_C$  to low temperature of  $60^\circ\text{C}$ . As Kell and Hellicar [22] indicated, the substitution of  $\text{Ti}^{4+}$  ions by  $\text{Zr}^{4+}$  ions leads to a reduction in Curie temperature for  $\text{BaTiO}_3$ -based ceramics. However, the addition of Bi gives a movement to high temperature of  $135^\circ\text{C}$ . The curve of fitting-BBT–BTZ describes the possible temperature dependence of capacitance change of BBT–BTZ calculated from volume percent and dielectric constant using Lichnetecker law. However,

the actual BBT–BTZ  $\varepsilon$ - $T$  curve shows a high dielectric constant and stability that disagrees with the fitting curve shown in Fig. 6. This result may be ascribed to the tension between the two phases. During sintering, internal tension comes into being because the two phases have different coefficients of thermal expansion. The internal tension promotes the tetragonal distortion, which is associated closely with permittivity. The dielectric constant rises with the increase of tetragonality ( $c/a$  ratio). The  $c/a$  ratio of BBT–BTZ is larger obviously than those of BBT and BTZ, shown in Table 1 and that can explain the high permittivity of BBT–BTZ qualitatively. High stability is due to the diffusion of the two phases into each other, which always induces dielectric peaks broadening.

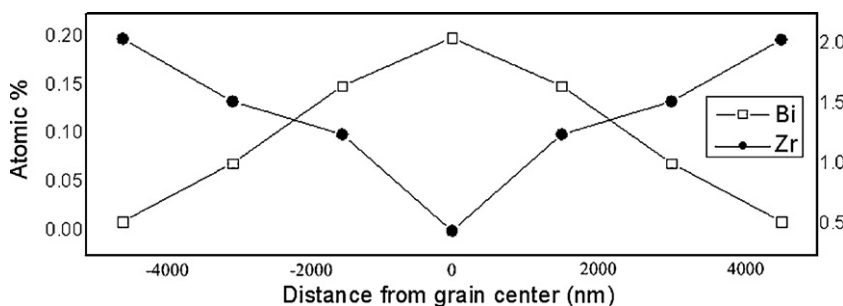


Fig. 4. EDX composition profile across the diameter of grain for BBT–BTZ sample.

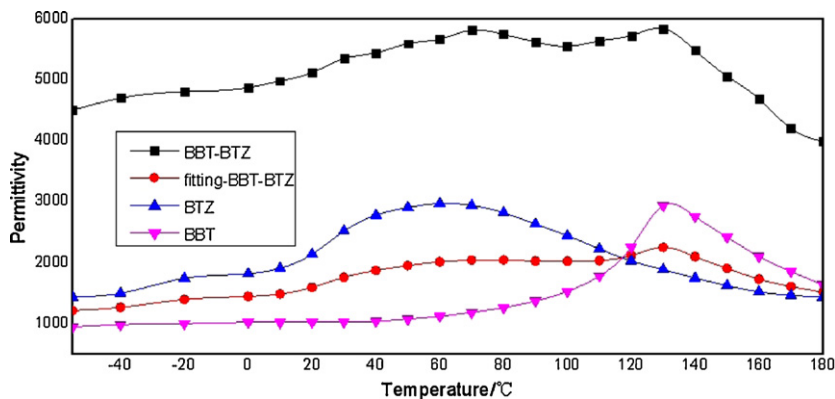


Fig. 5. Temperature dependence of capacitance change of  $\text{BaTiO}_3$ -based ceramic and the fitting of BBT and BTZ.

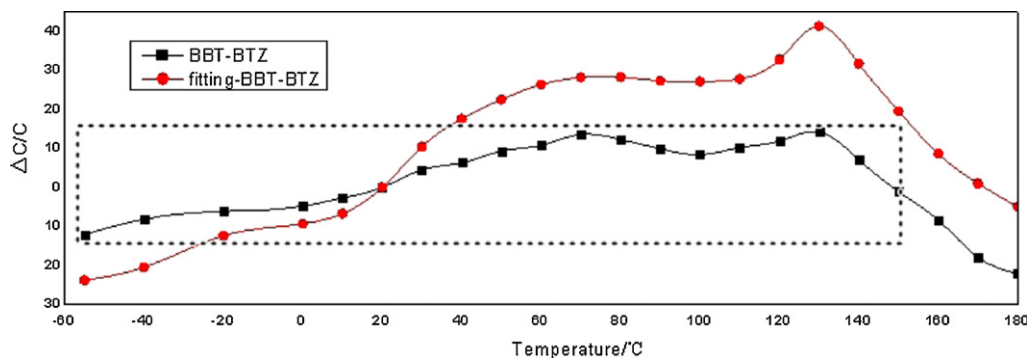


Fig. 6. Temperature coefficient of capacitance (TCC) of BBT–BTZ ceramic and fitting-BBT–BTZ.

#### 4. Conclusions

1. A new type of BaTiO<sub>3</sub>-based ceramic with hierarchical structure was designed. There were (Ba, Bi)TiO<sub>3</sub> and Ba(Ti, Zr)O<sub>3</sub> phases with different  $T_C$  coexisting in the ceramic grains from inside to outside. The phase composition is proved by XRD patterns, SEM photos and EDX profile. This demonstrates a promising avenue in the search for high performance capacitor materials with temperature-stability in the formula scheme “a ferroelectric ABO<sub>3</sub> + another ferroelectric ABO<sub>3</sub>”.
2. Hierarchical structure ceramic for X8R MLCC was prepared from (Ba, Bi)TiO<sub>3</sub>–Ba(Ti, Zr)O<sub>3</sub> powder, which is synthesized by wet chemical method under 100 °C. This method is simple, effective, low cost and easy maneuverability.
3. The dielectric constant and stability of (Ba, Bi)TiO<sub>3</sub>–Ba(Ti, Zr)O<sub>3</sub> ceramic is obviously superior to (Ba, Bi)TiO<sub>3</sub> and Ba(Ti, Zr)O<sub>3</sub>. The dielectric properties are:  $\varepsilon = \sim 6000$ ,  $\Delta C/C_{20\text{ }^\circ\text{C}}$  is –12.0%, 14.1, and –8.3% at –55, 130, and 160 °C, respectively, dielectric loss is less than 0.1.

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